Method for assessing unevenness of cellulose insulation layers aging of power transformers winding

Introduction. Improving the methods of estimating the insulation aging of the oil-immersed power transformer windings is an urgent task for transformer condition monitoring systems. The scientific novelty of the work is to take into account the uneven distribution of temperature and humidity along the vertical axis of the winding in modeling the aging of insulation and to develop methods for determining the conditions under which the aging rate of insulation in the intermediate layer will exceed aging rate in the hottest layer. The purpose of the work is to evaluate the wear unevenness of cellulose insulation based on modeling the distribution of temperature and humidity along the vertical axis of the power transformer winding. Methods. The transformer winding is mentally divided into horizontal layers of equal height, the reduction of service life is calculated in parallel for all horizontal layers. Layer with the maximum degree of aging for the entire period of operation and storage of the transformer is recognized as determining the reduction in the service life of the insulation of the transformer as a whole. A model of the interaction of winding layers is developed, with determination of temperatures, humidity, relative rate of aging of each layer due to temperature and humidity as a function of traditional design parameters such as load, cooling temperature, heat capacity and thermal resistance of transformer. The index of exceeding the aging rate by the layered method in comparison with this rate for the hottest layer is offered. The method of genetic algorithms determines the conditions for obtaining the maximum value of this index. Results. A computer model has been developed to predict the aging of the cellulose insulation by transformer windings. According to the proposed method, a layer with significantly shorter insulation aging time (in the example, time reduced by 39.18 %) than for the upper layer was determined, which confirms the feasibility of layer-by-layer monitoring and modeling of insulation aging processes of power oil-immersed transformer windings. References 25, tables 2, figures 4.

Key words: power oil-immersed transformer, cellulose insulation aging, computer model of layer-by-layer aging of winding insulation.
Known thermodynamic models are built on the basis of various differential equations of the heat balance of the transformer, which use various transformer equivalent circuits [11, 12]. Solutions of these equations are found both by analytical methods [13] and by computer simulation [11, 14-16].

Thermal modeling techniques are based on dynamic analogies of electrical and thermal processes, Computational Fluid Dynamics (CFD) and Thermal Hydraulic Network Model (THNM). Models based on the first technique do not take into account the nonlinear dependences of transformer thermal parameters. Models based on the other mentioned techniques require large computing resources and expensive commercial software for implementation.

The basic model for assessing the rate of insulation aging is the Montsinger equation [17], which determines the instantaneous rate of relative thermal aging of the insulation. Integration of this rate in a certain time interval gives the value of thermal aging of the insulation in this interval. The corresponding expression is called the «aging integral». Over time, multipliers were added to the aging integral, taking into account the influence on the cellulose insulation aging rate of its humidity, as well as the acid number of transformer oil [9, 11]. In other studies [4], these factors are taken into account in the expression of the aging rate through the values of the activation energy $E$ and the pre-exponential factor $A$, due to the influence of humidity, acids, and oxidation.

There are studies in which the influence of the humidity of cellulose insulation on the deterioration of its technical condition is experimentally confirmed [18, 19].

At the same time, the known models of insulation aging do not take into account the relationship between the temperature and moisture distribution in the winding insulation along its vertical axis. The intensity of transformer insulation aging is determined by the hot-spot temperature (HS) which is located in the upper part of the winding. Accordingly, it is assumed that the greatest service life reduction also occurs at the top of the transformer. On the other hand, the aging rate of cellulose insulation, in addition to temperature, is affected by the degree of cellulose humidity and the oxidation of transformer oil. It is known that the wettest spot, (WS) in an operating transformer is located in the lower part of the winding.

In [20], the concept of the most resource consumption spot (RCS) is introduced, it is shown that this spot may not coincide with the HS and WS spots, can change its position in the direction of the vertical axis of the winding depending on the dynamics of the load current of the transformer, humidity of cellulose insulation and other factors.

During the simulation of temperature and humidity distributions, the transformer winding with height $H$ is mentally divided into $N$ layers of the same height, as it shown in Fig. 1.

The number of layers is chosen in such a way that, within each layer, changes in temperature and humidity along the vertical axis of the winding can be neglected [20].

Winding layers are numbered from bottom to top. In this case, the $n$-th layer number ($1 \leq n \leq N$) characterizes the excess of the layer boundaries over the bottom of the winding. The excess of the upper $h_n$ and lower $h_b$ boundaries of the $n$-th layer is determined by the expressions:

$$h_n = \frac{Hn}{N}; \quad h_b = \frac{H(n-1)}{N}.$$

Thus, in the case of a change in the value of $N$ (for sufficiently large $N$), the excess of $h$ will correspond to another layer. For example, with $H = 2$ m and $N = 10$, the point located at a height of 1.4 m lies on the boundary of the seventh, and with $N = 20$, the 14th layer.

Due to the oppositely directed temperature and humidity gradients in the layers, accelerated aging of the different winding layers at different points in time is possible.

Therefore, it is necessary to take into account the aging rate of the insulation for each layer and, by integration, determine the most aged layer since the manufacture of the transformer. It can be assumed that the aging of this layer determines the aging of the winding insulation as a whole.

It should be noted that in the layered model given in [16] there is no mechanism for the interaction of the processes of dynamic redistribution of temperatures and humidity of cellulose along the vertical axis of the winding. This, in turn, does not allow performing computer simulation of layer-by-layer aging of insulation under non-stationary load conditions of the transformer.

The purpose of this work is to evaluate the aging unevenness of cellulose insulation based on modeling the distribution of temperature and humidity along the vertical axis of the winding of power transformers.

The task of the work is to develop a computer model for calculating the reduction in the service life of winding insulation layers based on the current values of the transformer load, ambient temperature, winding humidity and thermodynamic parameters of the transformer, as well as to develop a methodology for determining conditions under which cellulose insulation aging in the intermediate layer is greater than in the layer with the hottest spot.

Layer-by-layer model of power oil-immersed transformers cellulose insulation aging. To solve the set tasks, a computer layer-by-layer thermo- and moisture-dynamic model of the transformer is proposed. The structure of the model is shown in Fig. 2. The model as a whole and its elements are external models (black box models), that is, models that establish the dependence of outputs on inputs without detailing the physical processes in the transformer and in its parts.
The model consists of the unit for the formation of operating conditions, models of layers and units for determining the layer-by-layer insulation aging.

The operating conditions formation unit sets the values of the transformer load currents, the ambient temperature and the amount of moisture penetrating into the transformer tank. The layer model determines the input power, temperature and absolute humidity in the layer at the boundary of the «cellulose insulation-transformer oil» system. According to these data, the unit for determining the layer-by-layer aging of the insulation calculates the instantaneous rate of relative aging and the value of the aging of the cellulose insulation in the layer in accordance with the «aging integral» [4, 9-11].

Thus, the layer model consists of the input power model, thermodynamic and moisture dynamic models.

The input power of the \( n \)-th layer is determined from the expression [1]:

\[
P_{in,n} = \frac{P_{in}}{N} = \frac{I^2Z + P_l}{N}, \tag{1}
\]

where \( P_{in} \) is the transformer power losses, W; \( I \) is the load current, A; \( Z \) is the winding resistance, \( \Omega \); \( P_l \) is the no-load loss, W; \( N \) is the number of layers.

The thermodynamic model of the \( n \)-th layer is based on the heat balance equation in the winding cellulose insulation layer immersed in transformer oil. In the proposed model, the differential equation of the first degree is chosen as the heat balance equation:

\[
\frac{d\theta_n}{dt} = \frac{P_{in,n}}{C_n} - \frac{1}{C_nR_n}(\theta_n - \theta_{n-1}), \tag{2}
\]

where \( \theta_n, \theta_{n-1} \) is the temperature of the \( n \)-th, \((n-1)\)-th layer, \( ^\circ\text{C} \); \( d\theta_n/dt \) is the time derivative of the temperature of the \( n \)-th layer; \( C_n \) is the heat capacity of the \( n \)-th layer, \( \text{J/K} \); \( R_n \) is the thermal resistance of the \( n \)-th layer, \( \text{K/W} \).

A feature of the thermodynamic model of each layer is that it describes the thermal balance between the thermal power that is released in the layer winding as a result of the flow of load current and no-load losses and the thermal power that is transmitted through the moving oil to the overlying layers of the winding. Taking into account the direction of oil movement in the transformer tank from bottom to top, the thermal energy received by oil in the lower layer is involved in heating all layers of the winding. At the same time, the thermal energy released in the intermediate layer does not participate in the heating of the underlying layers of the winding. We also note that the oil heated in the \( N \)-th (upper) layer enters the cooler inlet, in which the oil temperature drops to the value \( \theta_0 \) and contacts the lower layer of the winding.

To determine the values of parameters – heat capacity \( C_n \) and thermal resistance \( R_n \) of the \( n \)-th layer, methods of comparing these parameters with the results of thermal tests or transformer condition monitoring were used [21].

The method takes into account the conditions (load current, ambient temperature, cooling modes) and the results (temperature of the upper layer of transformer oil, thermal constant of the transformer) of thermal tests. These parameters determine the requirements for the coefficients of the computer model of the heat balance equation of the transformer as a material point.
\[
\frac{d\theta_m}{dt} = \frac{P_{m\text{in}}}{C_n} - \frac{1}{C_n R_m} (\theta_m - \theta_a), \tag{3}
\]
where \(d\theta_m/dt\) is the time derivative of the top oil temperature; \(\theta_m\) is the top-oil temperature, \(^\circ\text{C}\); \(\theta_a\) is the ambient temperature, \(^\circ\text{C}\); \(P_{m\text{in}}\) is the input thermal power (power loss), W; \(C_n\) is the heat capacity of the transformer, J/K; \(R_m\) – thermal resistance of the transformer, K/W.

The values of the equation coefficients of this model are chosen experimentally to ensure that the simulation results coincide, with a given accuracy, with the results of thermal tests.

If during transformer operation the current value of the thermal parameters changes over time, then it is advisable to use condition monitoring data to determine the thermal parameters. For this purpose, we substitute the results of measuring the top-oil temperature and the ambient temperature for two points in time into the heat balance equations (3). Then we solve the resulting system of algebraic equations with respect to the coefficients of the original differential equation – the heat capacity and thermal resistance of the transformer [21].

At the next stage, the equation (2) coefficients are expressed in terms of the equation (3) coefficients. The following assumptions are taken into account:
1. Top-oil temperatures in these models must be equal. I.e. \(\theta_m = \theta_a\).
2. The lower layer inlet receives oil from the cooler outlet, which has a temperature \(\theta_l\). The moisture content of the oil in the cooler does not change.
3. The thermal resistance \(R_n\) of the section «cellulose insulation-transformer oil» in the layer model is expressed through the thermal resistance \(R_m\) of the transformer model as a material point:
\[
R_n = R_m (N + 1 - n) \quad \text{g}, \tag{4}
\]
where \((N + 1 - n)\) reflects the increase in thermal resistance \(R_n\) relative to the resistance \(R_m\); \(g\) is an empirical coefficient that takes into account the decrease in the thermal resistance of the «winding layer-transformer oil» section of the layered model compared to the thermal resistance of the «top oil layer-environment» section of the «single point» model, which is used to adjust the layered model.

As follows from (4), when \(n\) increases, \(R_n\) decreases and, consequently, the dissipated power in the layer increases. This leads to a decrease in the power going to the heating of the layer substance and a decrease in the layer temperature increment.

4. The heat capacity of the layer and the thermal power that is released in the layer \(n\) is \(N\) times less than the corresponding values of the transformer model as a material point:
\[
C_n = \frac{C_m}{N}; \quad P_{n\text{in}} = \frac{P_{m\text{in}}}{N}. \tag{5}
\]
After substituting expressions \((4) – (6)\) in (2) we get:
\[
\frac{d\theta_n}{dt} = \frac{P_{n\text{in}}}{C_m} - \frac{N g}{C_n R_m (N + 1 - n)} (\theta_n - \theta_{n-1}), \tag{6}
\]
where \(W(n) = A_w e^{-B_w \cdot \theta_n} \cdot p \cdot k \cdot \theta_n\),
\[
W(n) = A_w e^{-B_w \cdot \theta_n} \cdot p \cdot k \cdot \theta_n,
\]
where \(W(n)\) is the calculated humidity of cellulose insulation of the \(n\)-th layer, %; \(A_w, B_w, k, \theta_n\) are the empirical coefficients [24]; \(\theta_n\) is the temperature of the \(n\)-th layer of the transformer winding, \((n = 1, N), ^\circ\text{C}\); \(p\) is the partial pressure of water vapor, mmHg.

The value of the relative humidity of oil at the temperature of the \(n\)-th winding layer \(\theta_n\), %.

Relative humidity at \(\theta_n\) is determined from the expression [24]:
\[
\varphi' = \frac{W_m}{C_n(\theta_n)},
\]
where \(C_n(\theta_n)\) is the limiting humidity of oil at the temperature of the \(n\)-th layer, g/t; \(W_m\) is the absolute humidity of oil, taking into account the temperature of the \(n\)-th layer, g/t.

Thus, the moisture-dynamic model of the layer determines the absolute humidity in the layer based on the temperature value \(\theta_n\).

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for a time significantly longer than its thermal constant. In this case, the temperature \( \theta_{th} \) of the upper oil layers was constantly measured. According to the measurement data, the temperature of the excess of the upper oil layers \( \Delta \theta = 40 \, ^\circ C \) and the thermal time constant \( \tau = 2.4 \) hours were established. Based on these data and the passport value of the no-load loss parameter \( P_{0} \), the coefficients \( C_{m}, R_{m} \) of equation (3) were determined using the method [21, 25]. To solve equation (3), a computer model was used in the Simulink environment with the values of the input variables corresponding to the conditions of the thermal tests performed. The deviations of the values of \( \tau \) and \( \Delta \theta \) obtained as a result of modeling from the results of thermal tests do not exceed 5 %.

At the next stage, using this computer model, the temperature of the upper oil layers was determined for the conditions of the experiment with a layered model (Fig. 2): the load current \( I_{L} \) changed according to the profile shown in Fig. 3, and the temperature \( \theta_{th} \) is taken equal to 40 \( ^\circ C \). Further, the parameters of the layered model, in particular, the coefficient \( g \), were selected in such a way (\( g = 11.11 \)) that the temperature of the upper oil layers in the layered model was equal to the corresponding temperature of the original «one-point» model. After that, the temperatures obtained in the course of modeling using a layered model were used to determine the moisture distributions and aging rates.

The moisture content of cellulose insulation was calculated for the following initial data: \( A_{w} = 6.1; B_{w} = 0.04; k_{w} = 0.33; a_{w} = 0.0033 \) (empirical coefficients correspond to K-120 cable paper [24]). The mass of cellulose insulation of the transformer is assumed to be 6 tons, the mass of transformer oil is 47 tons. The graphs of changes in the parameters of these processes obtained as a result of modeling are shown in Fig. 3.

The steady-state values of temperatures, humidity, rates of relative aging of cellulose insulation and the aging itself in the layers of the model are given in Table 1.

<table>
<thead>
<tr>
<th>Layer</th>
<th>( \theta(n) ), ( ^\circ C )</th>
<th>( W(n) ), %</th>
<th>( v_{g} )</th>
<th>( v_{w} )</th>
<th>( v_{g} - v_{w} )</th>
</tr>
</thead>
<tbody>
<tr>
<td>10</td>
<td>91.10</td>
<td>0.846</td>
<td>0.4403</td>
<td>2.2545</td>
<td>0.9927</td>
</tr>
<tr>
<td>9</td>
<td>89.90</td>
<td>0.877</td>
<td>0.4111</td>
<td>2.3912</td>
<td>0.9830</td>
</tr>
<tr>
<td>8</td>
<td>88.86</td>
<td>0.913</td>
<td>0.3485</td>
<td>2.5588</td>
<td>0.8917</td>
</tr>
<tr>
<td>7</td>
<td>86.55</td>
<td>0.980</td>
<td>0.2666</td>
<td>2.8323</td>
<td>0.7551</td>
</tr>
<tr>
<td>6</td>
<td>83.23</td>
<td>1.089</td>
<td>0.1830</td>
<td>3.2981</td>
<td>0.6036</td>
</tr>
<tr>
<td>5</td>
<td>78.80</td>
<td>1.250</td>
<td>0.1120</td>
<td>4.0648</td>
<td>0.4553</td>
</tr>
<tr>
<td>4</td>
<td>73.27</td>
<td>1.480</td>
<td>0.0609</td>
<td>5.2739</td>
<td>0.3212</td>
</tr>
<tr>
<td>3</td>
<td>66.61</td>
<td>1.800</td>
<td>0.0292</td>
<td>7.1129</td>
<td>0.2077</td>
</tr>
<tr>
<td>2</td>
<td>58.82</td>
<td>2.237</td>
<td>0.0123</td>
<td>9.8245</td>
<td>0.1208</td>
</tr>
<tr>
<td>1</td>
<td>49.97</td>
<td>2.800</td>
<td>0.0045</td>
<td>13.7142</td>
<td>0.0617</td>
</tr>
</tbody>
</table>

From the results obtained it follows:
- under these conditions, the most consumable resource and the most heated is the upper layer of the transformer winding;
- the increase in temperature and humidity from layer to layer is not a constant value. That is, the functions \( \theta(n) \) and \( W(n) \) are non-linear.

The following notation is used: \( \theta_{\max} = \theta(N); \theta_{\min} = \theta(1); \Delta \theta = (\theta_{\max} - \theta_{\min}); W_{\max} = W(1); W_{\min} = W(10); \Delta W = W_{\max} - W_{\min}. \)

Using the simulation results, the coefficients of temperature change relative to the maximum values and humidity relative to the minimum values in the winding are calculated:

\[
k_{\theta}(n) = \frac{\theta_{\max} - \theta(n)}{\Delta \theta}; \quad k_{W}(n) = \frac{W(n) - W_{\min}}{\Delta W}.
\]

The obtained dependencies \( k_{\theta}(n) \) and \( k_{W}(n) \) are approximated by polynomials of the third degree. These polynomial functions and the resulting quality of approximation are shown in Fig. 4. Approximation quality was assessed using the determination coefficient \( R^2 \). The calculated values of \( R^2 \) are close to 1, which indicates a sufficient quality of the approximation.

Using the obtained dependencies of the coefficients \( k_{\theta}(n) \) and \( k_{W}(n) \), the dependences of the temperature \( \theta(n) \) and humidity \( W(n) \) of the layer as a function of \( \theta_{\max}, \Delta \theta, W_{\min}, \Delta W \) and \( n \) are obtained:

\[
\theta(n) = \theta_{\max} - \Delta \theta \cdot k_{\theta}(n) \quad \text{(8)}
\]

\[
W(n) = W_{\min} + \Delta W \cdot k_{W}(n). \quad \text{(9)}
\]

When assessing the rate of relative aging of the insulation, the hot-spot temperature of each layer was used, which is determined by the expression:

\[
\theta_{h}(n) = \theta(n) + \Delta \theta_{h}, \quad \text{(10)}
\]

where \( \Delta \theta_{h} \) is the temperature rise of the winding above the oil temperature in this \( (n-th) \) layer, which, in accordance with the recommendations of IEC [4], is assumed to be 22 \( ^\circ C \) for all layers.
The values of $W(n)$ and $\theta_k(n)$ from expressions (9) and (10) are substituted into the expressions for determining the rates of relative insulation aging. As a result of the action of temperature [6, 7]:

$$V_\theta(n) = 2 \frac{(\theta_k(n) - 98)}{6}$$  \hspace{1cm} (11)

and humidity

$$V_W(n) = \left( \frac{W(n)}{W_{BASE}} \right)^{1.493}$$  \hspace{1cm} (12)

where $W_{BASE}$ is the base humidity of cellulose insulation, %.

The designation for the product of the relative rates of thermal and moisture aging of insulation for layers $n$ and $N$ has been introduced:

$$V_n = V_\theta(n) \cdot V_W(n) ;$$  \hspace{1cm} (13)

$$V_N = V_\theta(N) \cdot V_W(N) .$$  \hspace{1cm} (14)

Evaluation of the effectiveness of the proposed method is based on the assumption that there is some non-top ($n$-th) layer with a higher insulation aging rate than in the top layer ($N$-th). Without taking this fact into account, we underestimate the intensity of insulation aging. Thus, the conditions under which the resource is underestimated are determined from the expressions:

$$V_N < V_n$$  \hspace{1cm} (15)

or

$$V_N - V_n < 0.$$  \hspace{1cm} (16)

In this case, it is assumed that $V_N$ and $V_n$ are positive and different from zero and infinity. The following index is proposed:

$$F = \frac{V_N}{V_n} .$$  \hspace{1cm} (17)

Then condition (15) can be rewritten in the form:

$$F < 1$$  \hspace{1cm} (18)

Moreover, the greatest underestimation of the aging intensity is achieved with a minimum index $F$. Substituting expressions (11-14) into expression (17), we obtain an expression for determining $F$:

$$F = \frac{V_N}{V_n} = \frac{V_\theta(N) \cdot V_W(N)}{V_\theta(n) \cdot V_W(n)} = \frac{V_\theta(N)}{V_\theta(n)} \cdot \frac{V_W(N)}{V_W(n)} ,$$  \hspace{1cm} (19)

where

$$\frac{V_\theta(N)}{V_\theta(n)} = \frac{\left( \frac{W(N)}{W_{BASE}} \right)^{1.493} - \frac{\left( \frac{W(n)}{W_{BASE}} \right)^{1.493}}{\left( \frac{W(n)}{W_{BASE}} \right)^{1.493}}}{\left( \frac{W(n)}{W_{BASE}} \right)^{1.493} - \left( \frac{W(n)}{W_{BASE}} \right)^{1.493}} \geq 1 ;$$  \hspace{1cm} (20)

$$\frac{V_W(N)}{V_W(n)} = \frac{\frac{W(N)}{W_{BASE}}}{\frac{W(n)}{W_{BASE}}} = \left( \frac{W(N)}{W(n)} \right)^{1.493} .$$  \hspace{1cm} (21)

Substituting (20, 21) into (19), taking into account (8), (9) and approximation results in Fig. 4, we obtain:

$$\frac{V_\theta(N)}{V_\theta(n)} = \frac{\left( \frac{W(N)}{W_{BASE}} \right)^{1.493} - \frac{\left( \frac{W(n)}{W_{BASE}} \right)^{1.493}}{\left( \frac{W(n)}{W_{BASE}} \right)^{1.493}}}{\left( \frac{W(n)}{W_{BASE}} \right)^{1.493} - \left( \frac{W(n)}{W_{BASE}} \right)^{1.493}} \geq 1 ;$$  \hspace{1cm} (22)

$$\frac{V_W(N)}{V_W(n)} = \left( \frac{\frac{W(N)}{W_{BASE}}}{\frac{W(n)}{W_{BASE}}} \right)^{1.493} .$$  \hspace{1cm} (23)

Analysis of expressions (15) and (16) shows that:

$$V_N < V_n \leq 1$$  \hspace{1cm} and  $$V_N - V_n \geq 1 .$$

Therefore, the $F$ index can be either less or greater than 1. When $F > 1$, the greatest insulation aging occurs in the upper layer of the winding.

To determine the conditions under which $F_{\min}$ is achieved, the method of genetic algorithms [23] was applied. In accordance with this method, expression (19), taking into account expressions (22) and (23), is a fitness function, the minimum of which is to be determined.

The search for $F_{\min}$ was carried out using the ga function from the MATLAB software package. The initial restrictions on the input variables, the obtained value $F_{\min}$ of the value of the input parameters and the number of the layer at which $F_{\min}$ is reached are given in Table 2. This is a method of finding a function extremum by directional iteration of the values of the function arguments. Its advantage is that it does not impose requirements on the complexity of the function.

<table>
<thead>
<tr>
<th>Name, designation, unit measurements, variable type</th>
<th>Value range</th>
<th>Value for $F_{\min}$</th>
<th>$F_{\min}$ value</th>
<th>Layer number</th>
</tr>
</thead>
<tbody>
<tr>
<td>Number of layers, $N$, pieces, integer</td>
<td>$N=10$</td>
<td>10</td>
<td>0.6182</td>
<td>8</td>
</tr>
<tr>
<td>Oil temperature range, $\Delta\theta$, °C, real</td>
<td>$20&lt;\Delta\theta&lt;60$</td>
<td>20</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Absolute humidity of the upper layer, $W(N)$, %, real</td>
<td>$0.3&lt;W(N)&lt;1$</td>
<td>0.3</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Winding humidity change range, $\Delta W$, %, real</td>
<td>$0&lt;\Delta W&lt;1.5$</td>
<td>1.5</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Fig. 4. Graphs of dependencies: $a - k_\theta(n)$; $b - k_W(n)$
As can be seen from Table 2, the value of the index $F_{\text{min}} = 0.6182$ obtained during the operation of the genetic algorithm takes place for the eighth layer. From here, according to expression (17):

$$V_n = V_N / F_{\text{min}} = 1.6176 \cdot V_N.$$  

(24)

Thus, the adjusted value of the insulation aging rate is 61.76% higher than that calculated by the original method. If we assume that the wear rates $V_n$, $V_N$ have a constant value, then the service life of the insulation will be reduced at these rates for different times. Wherein

$$V_{n,t_1} = V_{n,t_2}.$$  

(25)

where $t_1$, $t_2$ are expected service life of cellulose insulation of the $n$-th and upper ($N$-th) layers of the winding, respectively, years.

Since for $F_{\text{min}} < 1$ we have $V_n > V_N$, then $t_1 < t_2$. Then, taking into account (24) and (25), we have a reduction in the service life:

$$\Delta t = (t_2 - t_1) = t_2(1 - F_{\text{min}}).$$  

(26)

Where does the relative reduction in service life, expressed as a percentage, be defined as:

$$\Delta t / t_2(\%) = (1 - F_{\text{min}}) \cdot 100\% = (1 - 0.6182) \cdot 100\%. $$  

(27)

For example, with $t_2 = 10$ years and $F_{\text{min}} = 0.6182$ we get $\Delta t = 3,918$ years, $t_1 = 6,182$ years, $\Delta t / t_2 [\%] = 39.18\%$. That is, the calculation of the resource consumption time rate according to the proposed method gives a significantly lower (in the example by 39.18%) residual insulation life.

Conclusions.

1. It has been established that the distribution in the layers of the winding of the average values of temperature and humidity of cellulose insulation in the direction of the vertical axis of the winding is multidirectional. Therefore, under certain conditions in which the insulation operates (for example, at high absolute humidity, a large temperature difference along the vertical axis of the winding, etc.), it is possible that the aging rate of the insulation under the action of temperature and moisture in the intermediate horizontal layer of the winding exceeds the aging rate in the layer with the most hot point, and as a result, greater wear of the intermediate layer.

2. The index $F$ is proposed for assessing the excess rate of aging of cellulose insulation under the influence of temperature and moisture.

3. Using the method of genetic algorithms, the maximum excess of the rate of relative wear of insulation in the intermediate layer $F_{\text{min}}$ was estimated under given restrictions on the parameters of temperature and moisture distribution, as well as the number of layers into which the transformer winding is mentally divided.

4. The method for determining the dynamics of the distribution of temperature and humidity along the vertical axis of the winding has been improved with experimentally obtained results of measurements of the ambient temperature, load current and calculated values of the thermophysical parameters of cellulose insulation, which makes it possible to improve the accuracy of assessing its technical condition.

5. The expressions obtained in the work for determining the index $F$ refer to one variant of estimates of the average rate of relative wear of insulation from among those presented in the known literature. Namely, ratings:

- for thermally unimproved cellulose insulation;
- with the determination of the thermal wear rate according to the Montsinger equation;
- taking into account the relationship of various factors (temperature, humidity, and others) in the form of a product of aging rates as a result of the action of one factor.

5. In the future, it is planned to obtain an analytical expression for determining the index $F$ for other assessment options: aging of paper insulation with improved thermal characteristics; determining the average rate of aging as a function of the activation energy $E$ and the pre-exponential factor $A$; an additive form of the relationship of average aging rates, taking into account individual factors.

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M.O. Poliakov1, Doctor of Technical Science, Professor, V.V. Vasylevskiy2, PhD
1 Zaporizhzhia Polytechnic National University, 64, Zhukovsky Str., Zaporizhzhia, Ukraine, 69063, e-mail: polyakov@zntu.edu.ua; lisses@ukr.net (Corresponding author)